

enable

mgis.fenics Part II: Cosserat media in small deformation with mgis.fenics

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AGENDA

- ❖ Introduction
- ❖ Cosserat media:
 - Motivation
 - Model
 - Implementation
- ❖ Performance
- ❖ Conclusion
- ❖ Next steps

Introduction

ENABLE H2020 project

This European Training Network actively involves academics and industrial partners in training a new generation of young researchers for the future of **manufacturing**. By developing new solutions for **metallic alloys**, ENABLE proposes a complete rethink of the usual process simulation methods. Innovative **multiscale** (from microscopic to macroscopic scales), and **multi-physics** (strong thermomechanical and microstructural couplings) are addressed.



Cosserat Media - Motivation

- Development of an **Adiabatic Shear Band**
- Localization phenomena & prediction of characteristic length and size effect
- aim to regularize the model and avoid mesh dependency

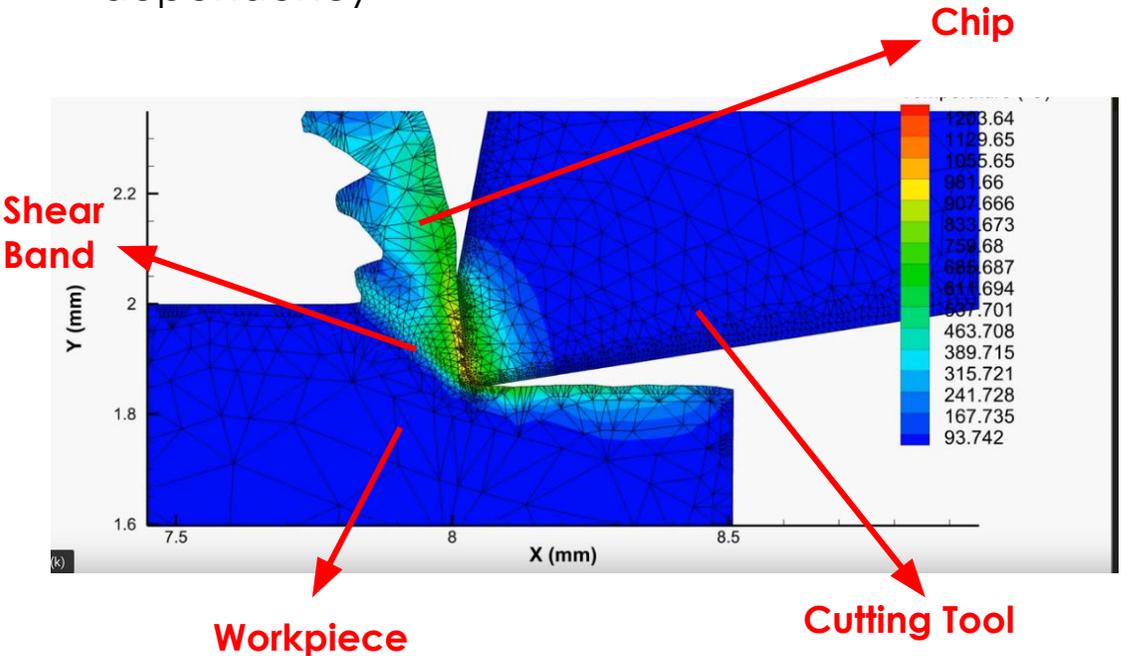


Fig.1 2D machining of Ti-6Al-4V - using Third Wave Systems AdvantEdge - Temperature

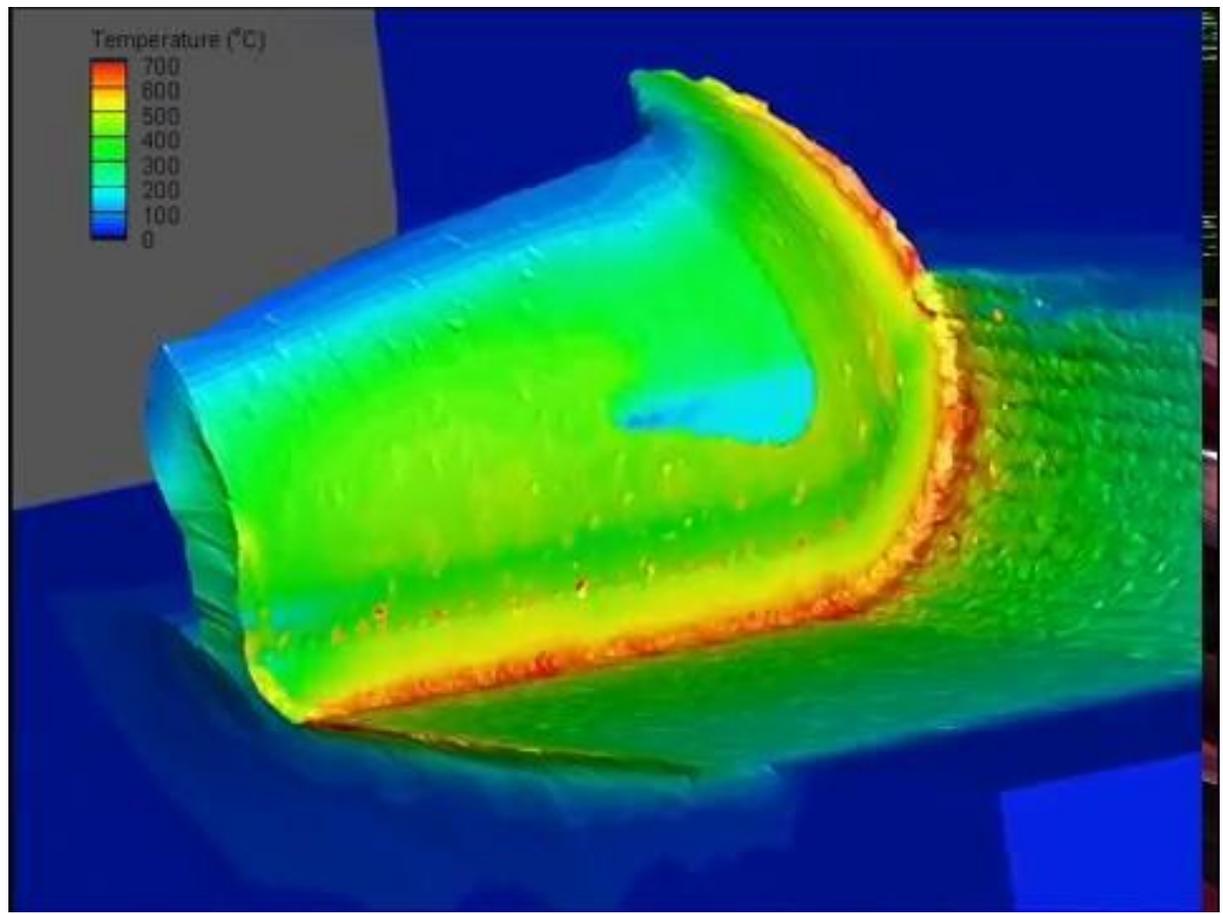


Fig.2 Chip formation during the machining of grade 316L stainless steel - using Third Wave Systems AdvantEdge - Temperature, courtesy of Sandvik Coromant

Cosserat Media in small deformation - model

- ❖ the model was initially introduced in 1909 by the Cosserat brothers [Cosserat 1909]
- ❖ Raffaele Russo has been working on formulating a thermodynamically consistent model for small deformation and large deformation [Russo et al. 2020]

Displacement \leftarrow $\{u_i, \theta_i\}, i = 1, 2, 3$ \rightarrow Extra degrees of freedom - the rotation of the microstructure

Deformation measures, where $\epsilon_{ijk} = \begin{cases} 1, & \text{if } (i,j,k) = (1,2,3), (2,3,1) \text{ or } (3,1,2); \\ -1, & \text{if } (i,j,k) = (3,2,1), (2,1,3) \text{ or } (1,3,2); \\ 0, & \text{otherwise.} \end{cases}$

$\underline{\mathbf{e}} = \underline{\mathbf{u}} \otimes \nabla + \underline{\underline{\epsilon}} \cdot \underline{\underline{\theta}}$ \rightarrow Cosserat deformation tensor

$\underline{\underline{\mathbf{k}}} = \underline{\underline{\theta}} \otimes \nabla$ \rightarrow Cosserat wryness tensor

Balance/equilibrium equation:

$$\int_{\Omega} \left(\underline{\underline{\boldsymbol{\sigma}}} : \underline{\dot{\mathbf{e}}} + \underline{\underline{\boldsymbol{\mu}}} : \underline{\dot{\mathbf{k}}} \right) dV = \int_{\Omega} \left(\underline{\mathbf{f}} \cdot \underline{\dot{\mathbf{u}}} + \underline{\mathbf{c}} \cdot \underline{\dot{\underline{\theta}}} \right) dV + \int_{\partial\Omega} \left(\underline{\mathbf{t}} \cdot \underline{\dot{\mathbf{u}}} + \underline{\mathbf{m}} \cdot \underline{\dot{\underline{\theta}}} \right) dS;$$

classical stress
couple stress
body force / couple
external surface / couple traction



Cosserat Media in small deformation - model

❖ Material model for elasto-plasticity

From the Helmholtz free energy and the Clausius-Duhem inequality (2nd thermodynamic law) we can verify the compatibility and derive the following:

- assuming single plastic multiplier we calculate using the consistency condition and the

normality rule:
$$\dot{p} = \frac{\underline{\mathbf{n}} : \underline{\underline{\Lambda}} : \underline{\dot{\mathbf{e}}} + \underline{\mathbf{n}}_c : \underline{\underline{\mathbf{C}}} : \underline{\dot{\mathbf{k}}}}{\frac{\partial A}{\partial p} + \underline{\mathbf{n}}_c : \underline{\underline{\Lambda}} : \underline{\mathbf{n}} + \underline{\mathbf{n}}_c : \underline{\underline{\mathbf{C}}} : \underline{\mathbf{n}}};$$

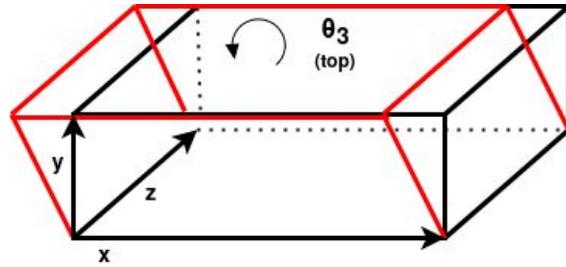
$$\frac{\partial f}{\partial \underline{\boldsymbol{\sigma}}} = \underline{\mathbf{n}} = \frac{3}{2} \frac{a_1 \underline{\boldsymbol{\sigma}}' + a_2 \underline{\boldsymbol{\sigma}}'^T}{\sigma_{eq}};$$

- Normals to the yield surface in the stress and couple stress spaces
$$\frac{\partial f}{\partial \underline{\boldsymbol{\mu}}} = \underline{\mathbf{n}}_c = \frac{3}{2} \frac{b_1 \underline{\boldsymbol{\mu}} + b_2 \underline{\boldsymbol{\mu}}^T}{\sigma_{eq}};$$
- Equivalent Stress as in [Borst 1991; Lippmann 1969; Mühlhaus and Vardoulakis 1987]

$$\sigma_{eq} = \sqrt{\frac{3}{2} (a_1 \underline{\boldsymbol{\sigma}}' : \underline{\boldsymbol{\sigma}}' + a_2 \underline{\boldsymbol{\sigma}}' : \underline{\boldsymbol{\sigma}}'^T + b_1 \underline{\boldsymbol{\mu}} : \underline{\boldsymbol{\mu}} + b_2 \underline{\boldsymbol{\mu}} : \underline{\boldsymbol{\mu}}^T)};}$$

Characteristic length:
$$l_p = \sqrt{\frac{a}{b}};$$

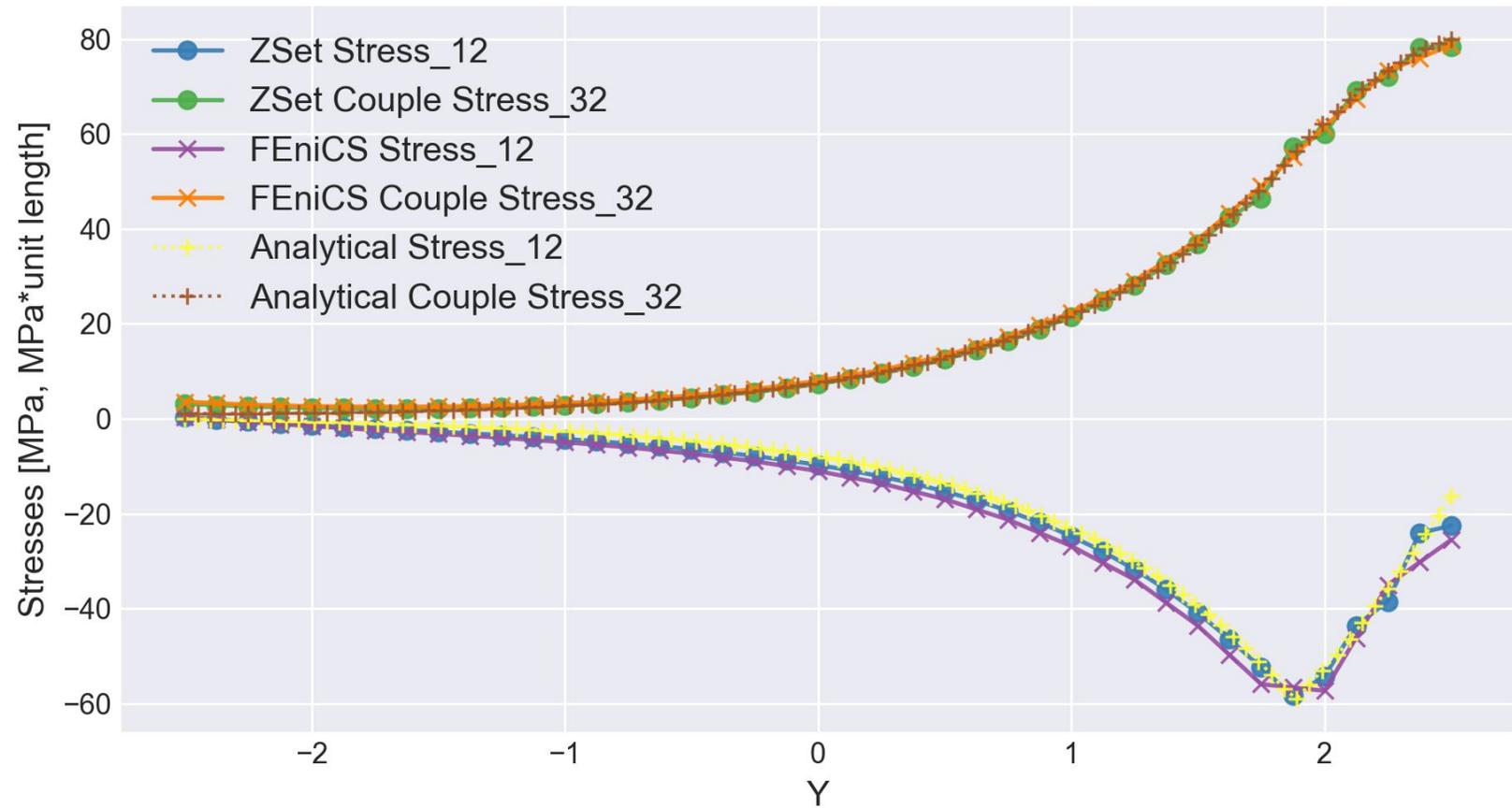
Cosserat Media Implementation - Glide test



Boundary Conditions

$u_3 = 0$ (whole)

$\theta_1 = 0$ (whole)
 $\theta_2 = 0$ (whole)
 $\theta_3 = 0.001$ (top)



Iterations to converge - equilibrium:

- FEniCS: [1,1,1,1,1,3,7,8,8,9,10,10,11,12,13,15,16,18]
- Zset:[1,1,1,1,1,4,5,6,6,6,7,7,8,9,10,10,9]

Fig.3 Comparison MFront+FEniCS with ZSet and the analytical solution [S.Forest et al.]

Cosserat Media Implementation

Fig. 5 Explicit Implementation MFront

$$\sigma_{eq} = \sqrt{\frac{3}{2} (a_1 \underline{\sigma}' : \underline{\sigma}' + a_2 \underline{\sigma}' : \underline{\sigma}'^T + b_1 \underline{\mu} : \underline{\mu} + b_2 \underline{\mu} : \underline{\mu}^T)}$$

```
@Derivative {
const auto se = 2 * mu * deviator(sym(εe1)) + mu_c * (εe1 - transpose(εe1));
const auto seq = sqrt(3 * (a_1 * (se | se) + a_2 * (se | transpose(se)) +
                        b_1 * (μk | μk) + b_2 * (μk | transpose(μk))) /
                    2);

d_tεe1 = d_teto;
d_tκe1 = d_tκ;
if (seq - R0 - H * p > 0) {
const auto n = eval(3 * (a_1 * se + a_2 * transpose(se)) / (2 * seq));
const auto n_c = eval(3 * (b_1 * μk + b_2 * transpose(μk)) / (2 * seq));
const auto cste = 1 / (H + (n | ∂σ/∂Δeto | n) + (n_c | ∂μk/∂Δκ | n_c));
d_t p = ((n | ∂σ/∂Δeto | d_teto) + (n_c | ∂μk/∂Δκ | d_tκ)) * cste;
d_tεe1 -= d_t p * n;
d_tκe1 -= d_t p * n_c;
}
}
```

$$\frac{\partial f}{\partial \underline{\sigma}} = \underline{n} = \frac{3}{2} \frac{a_1 \underline{\sigma}' + a_2 \underline{\sigma}'^T}{\sigma_{eq}}$$

$$\frac{\partial f}{\partial \underline{\mu}} = \underline{n}_c = \frac{3}{2} \frac{b_1 \underline{\mu} + b_2 \underline{\mu}^T}{\sigma_{eq}}$$

$$\dot{p} = \frac{\underline{n} : \underline{\Lambda} : \dot{\underline{e}} + \underline{n}_c : \underline{C} : \dot{\underline{k}}}{\frac{\partial A}{\partial p} + \underline{n}_c : \underline{\Lambda} : \underline{n} + \underline{n}_c : \underline{C} : \underline{n}}$$

Fig.5 .mfront file for the Cosserat glide test - continuation
 Optimization: converting to an implicit implementation

Cosserat Media Implementation

FEniCS + MFront



Zset

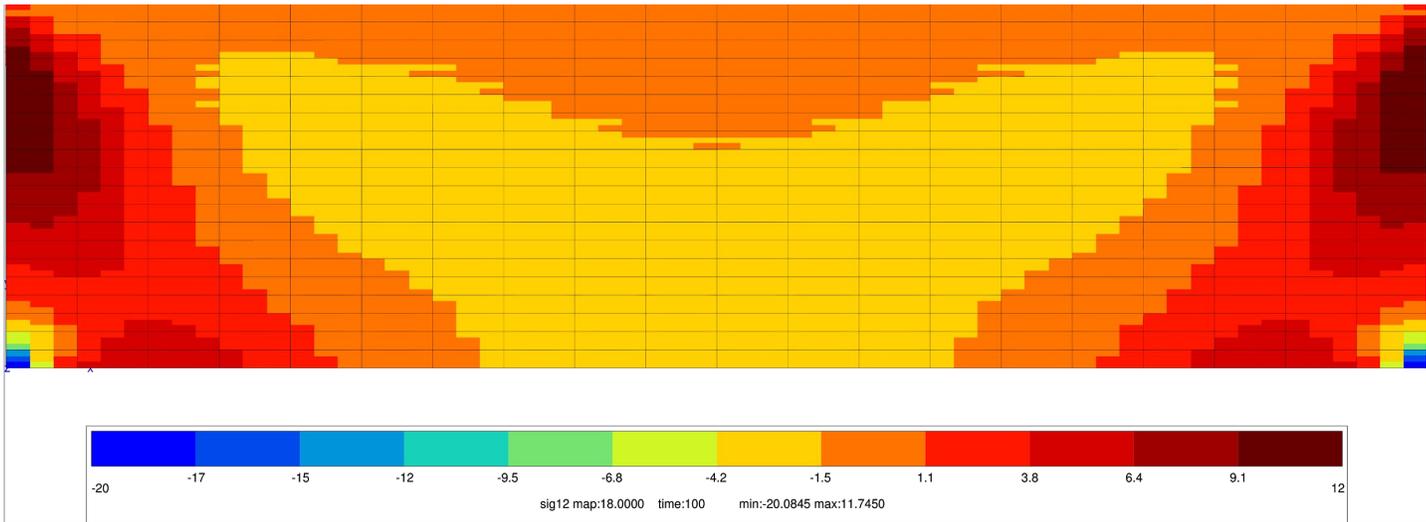
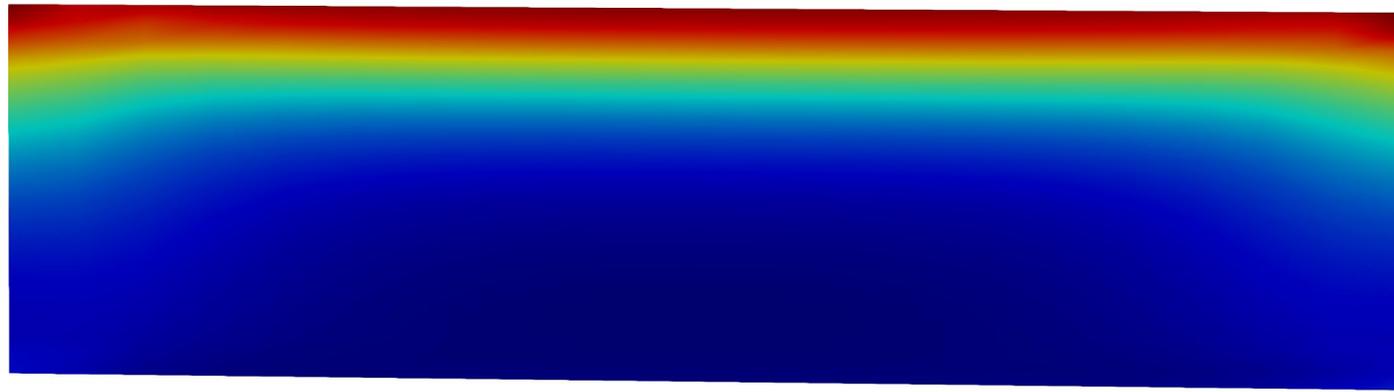


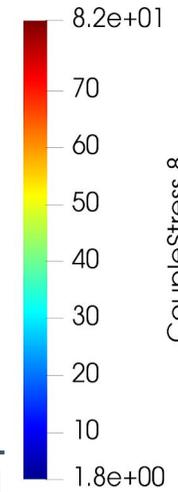
Fig.6
Glide test - Result
for the stress, σ_{12}

Cosserat Media Implementation

FEniCS + MFront



CoupleStress 8



Zset

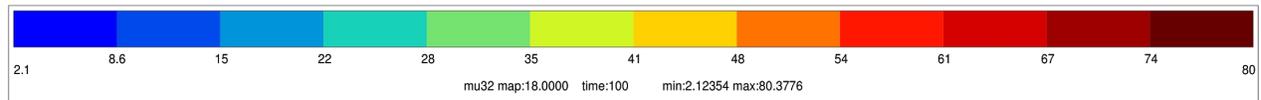
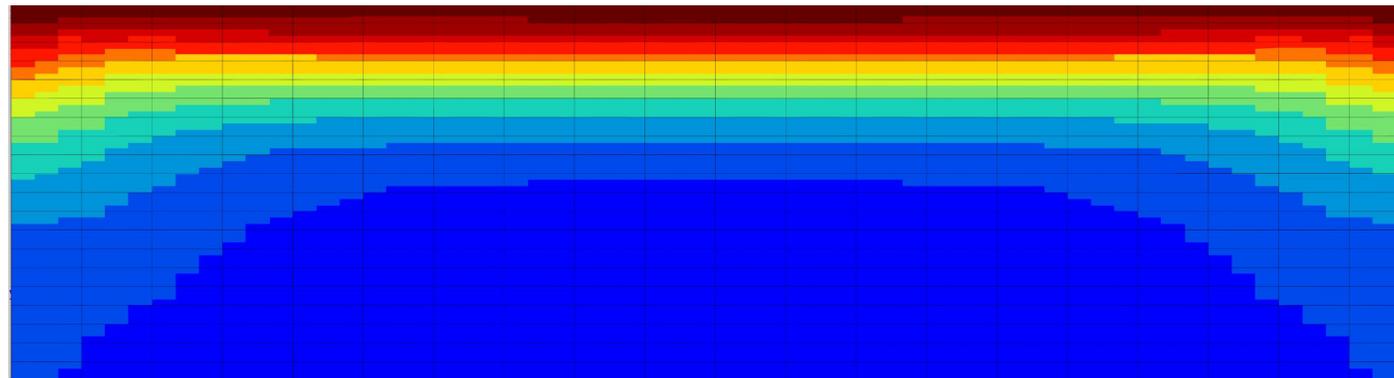
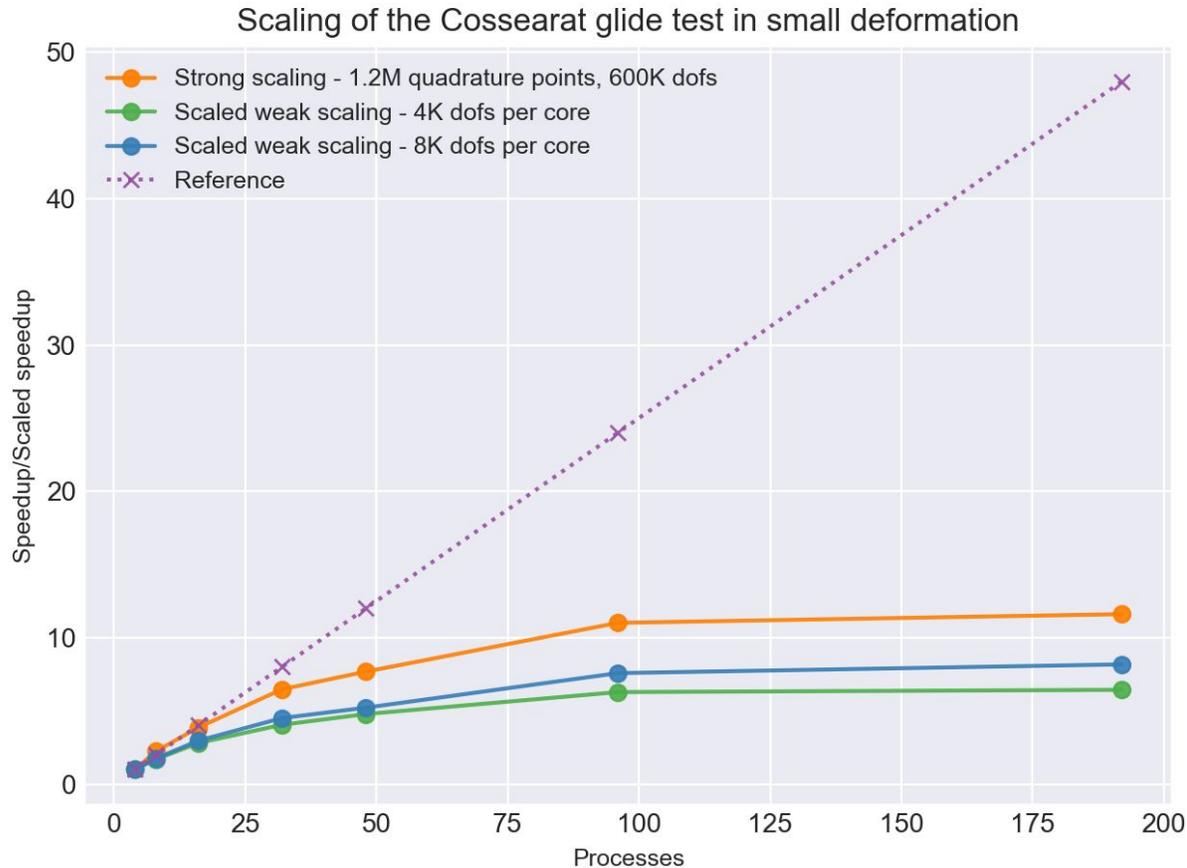


Fig.7
Glide test - Result
for the couple
stress, μ_{32}

Performance



ATLAS EDR @ Donostia International Physics Center

- Infiniband EDR network
- 37 nodes with Intel Xeon Platinum 8168 (24 cores per node x 2 threads)
- 8 nodes with Intel Xeon Platinum 8280 (28 cores per node x 2 threads)
- 2x NVIDIA Tesla P40, 1x NVIDIA Tesla P40

Current setup:

- using Singularity container
- using MPICH using the UCX network framework

Fig.8 Strong and weak scaling plot for the glide test

Conclusions

- From the profiling and scaling results we can conclude that the major bottleneck is the resolution of the system of nonlinear equations (quasi Newton line search) using MUMPS as a linear solver

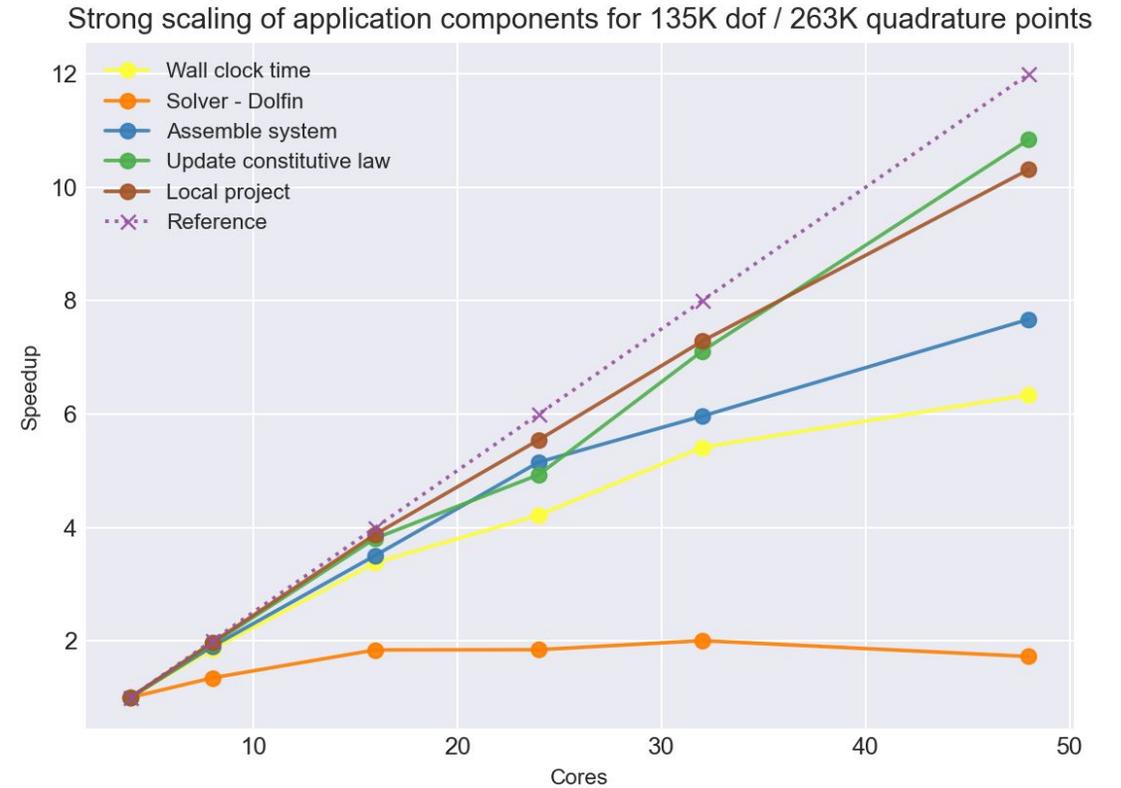
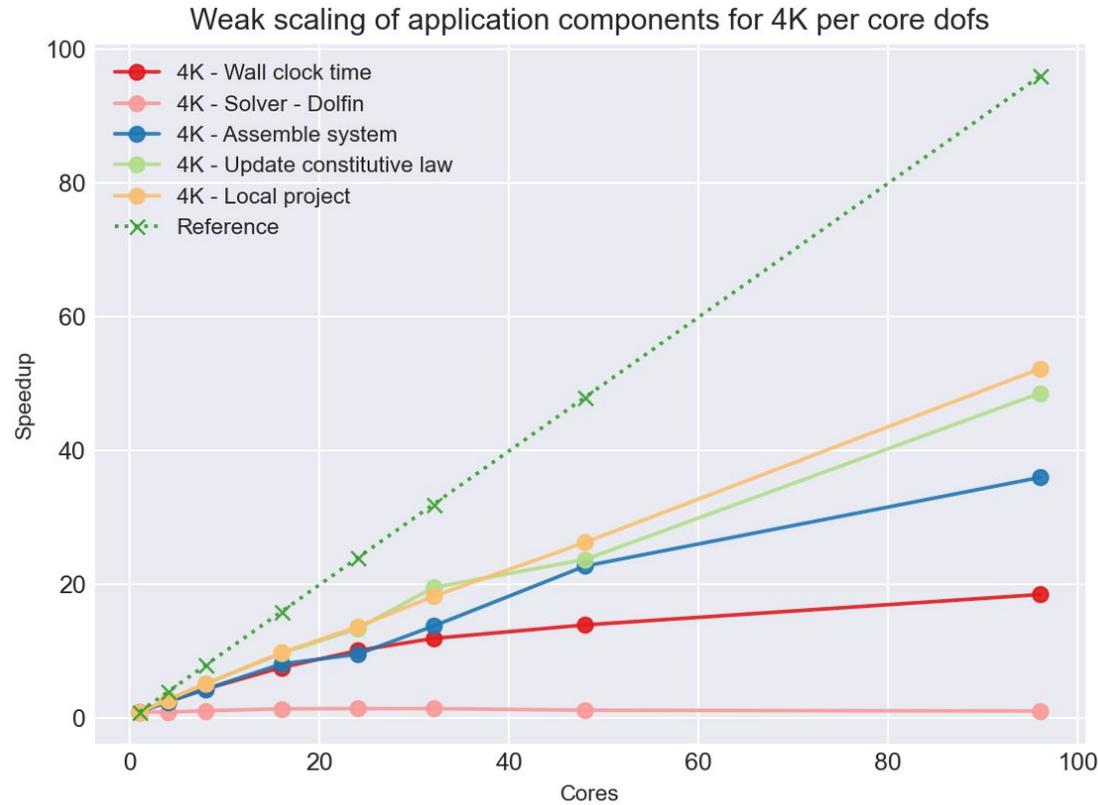


Fig.9 Strong and weak scaling plot for various routines part of the simulation

Next steps

- ❖ Increase problem size
- ❖ Native installation of the software stack on ATLAS-EDR
- ❖ Profiling with EXTRAE for MPI statistics, DCRAB for node statistics
- ❖ Exploring other linear solvers (and nonlinear)
- ❖ Implicit scheme implementation
- ❖ Porting to dolfin-x
- ❖ Further HPC analysis and code optimizations
- ❖ Implementation of the full thermodynamically consistent Cosserat model in Large deformation - elasto viscoplasticity

Questions



Thank you for your attention!